

Development of Analytical Methods for Free-MgO in Steelmaking Slag[†]

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Abstract:

Steelmaking slags have been widely used as aggregate for roadbeds and civil engineering. However, when used as aggregate, slag sometimes expands as a result of hydration, resulting in the evolution of cracks at the surface of roads. Because free magnesium oxide (free-MgO) as well as free calcium oxide in the slag are potential causes of this expansion, analytical methods to determine the free-MgO in slag for accurate evaluation of expansion are required. Based on a combination of chemical extraction and thermogravimetry (TG), an accurate method to determine the free-MgO in steelmaking slag was developed. In this method, the free-MgO and magnesium hydroxide ($\text{Mg}(\text{OH})_2$) in the steelmaking slag are dissolved in an ethyleneglycol solution containing iodine and ethanol when heated. The amount of the magnesium species dissolved in the solution is determined by inductively coupled plasma atomic emission spectroscopy (ICP-AES). The amount of $\text{Mg}(\text{OH})_2$ in the slag is determined separately by TG, and the result is then subtracted from that of the magnesium species dissolved in the ethyleneglycol to obtain the amount of free-MgO. The newly-established method enables determination of free-MgO in steelmaking slag at the 0.1 mass% level.

1. Introduction

Steelmaking slag, which is a byproduct of the steel manufacturing process, is used as a concrete aggregate, roadbed material, etc. Roadbed material made from steelmaking slag is used based on adequate consideration of the expansion of the slag¹⁾. Hydration of free

calcium oxide (free-CaO), free magnesium oxide (free-MgO), etc. in the slag is considered to be the main cause of this expansion^{2,3)}.

In order to understand the expansion mechanism of slag, it is important to determine the free-CaO and free-MgO in the slag. The analytical method by ethyleneglycol (EG) extraction⁴⁻⁷⁾ is widely known as a determination method for free-CaO. As determination methods that do not use chemical extraction, determination by X-ray diffraction (XRD)^{8,9)}, calculation from infrared spectroscopy after hydration with heavy water¹⁰⁾ and others have been reported. Reported methods for determination of free-MgO in slag include extraction by using ammonium nitrate¹¹⁾, the solid-state ²⁵Mg nuclear magnetic resonance (NMR) spectroscopy¹²⁾, calculation from infrared spectroscopy after hydration with heavy water¹³⁾, etc. Determination of free-MgO by ammonium nitrate extraction has the problems that Mg compounds other than MgO are also extracted or MgO is not extracted completely, leading to poor repeatability. The ²⁵Mg NMR spectroscopy is not a general-purpose method, as high performance NMR apparatus are necessary, and requires a long measurement time. The method of calculation from infrared spectroscopy after heavy water hydration also lacks practicality, since MgO must be changed completely to $\text{Mg}(\text{OH})_2$ by hydration, and considerable time is required.

On the other hand, determination of CaO and MgO using I_2 -EG solution and measuring the electrical conductivity before and after addition has been reported as an analytical method for CaO and MgO in cement clinker¹⁴⁾. The I_2 -alcohol dissolution method is known as a standard method for extraction of oxides in steel^{15,16)}.

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From the above, an I₂-alcohol-EG solution was considered to be a possible solvent for extraction of free-MgO in slag. However, there were no cases in which this solvent was studied as an analytical method for MgO in slag. Therefore, the authors investigated fractional determination of free-MgO in slag by chemical extraction using an I₂-alcohol-EG solution, and determined the optimum conditions for dissolution of free-MgO and Mg(OH)₂ by using standard reagents and actual slags. We also found that thermogravimetric analysis can be used in determination of Mg(OH)₂ that is dissolved together with MgO. This paper reports a determination method for free-MgO in slag which was developed based on the study outlined above.

2. Experimental

2.1 Reagents and Sample Materials

2.1.1 Reagents

The MgO used in this study was a high purity reagent manufactured by Kanto Chemical Co., Inc. The Mg(OH)₂ was a high purity reagent manufactured by Kojundo Chemical Laboratory Co., Ltd. As Al complex oxides, Si complex oxides and Fe complex oxides for use in investigation of the melting behavior of Mg oxides, Mg(AlO₂)₂, Mg₂Si₃O₈·5H₂O and MgFe₂O₄ manufactured by Wako Pure Chemical Industries, Ltd. and Kojundo Chemical Laboratory were used.

2.1.2 Slags

The steelmaking slags (Slag A-D) shown in **Table 1** were used in the study of free-MgO analysis. When used in analysis, the slags were crushed in advance to 0.075 mm or smaller.

2.2 Experimental Method

2.2.1 Melting and determination method for MgO+Mg(OH)₂ in slag

A 0.1 g sample of slag crushed to 0.075 mm or smaller is weighed in a conical flask (100 ml), and 17 ml of ethyleneglycol and 8 ml of 25 mass% I₂ ethanol are added to the flask. The flask is placed in a hot water

bath adjusted to 80±5°C and heated for 60 min while stirring with a stirrer. After heating for 60 min, the flask is cooled to room temperature in running water. Using a syringe with a tube attached to its tip, approximately 5 ml of extraction liquid is aspirated and discharged, and the syringe and inside of the tube are rinsed. After taking 5 ml or more of the extract, the tube is removed, a membrane filter (pore size: 0.45 μm) is attached, and filtration is performed. After discarding the first approximate 1 ml, the filter is rinsed. The following 1 ml of the filtrate is separated and transferred to a 100 ml volumetric flask. 10 ml of hydrochloric acid (1+1), 3 ml of ethanol, and 5 ml of internal standard solution Y (100 μg/ml) are added to the flask, and the contents are adjusted to a constant volume of 100 ml with water. The intensity of emission of Mg and Y in a calibration curve solution and in the sample solution is measured by an inductively coupled plasma-atomic emission spectrophotometer (ICP-AES), and the concentration of Mg in the sample solution is calculated by the Y internal standard method. Here, the obtained results take Mg as (MgO+Mg(OH)₂).

2.2.2 Determination of Mg(OH)₂ in slag

The Mg(OH)₂ contained in slag is determined by the following procedure.

(1) Removal of Ca(OH)₂

A 0.15 g sample of slag crushed to 0.075 mm or smaller is weighed in a conical flask (100 ml), and 25 ml of ethyleneglycol is added. The flask is placed in a hot water bath adjusted to 70±5°C and heated for 60 min while stirring with a stirrer. After heating for 60 min, the flask is cooled to room temperature in running water. The slag after filtration is rinsed with ethanol, and is then dried in a vacuum desiccator.

(2) Thermogravimetric analysis (TG)

The slag from which Ca(OH)₂ has been removed by the above-mentioned method is measured by TG under the following conditions.

Sample weight: 0.1 g

Atmosphere: Ar

Heating conditions: Room temperature to 500°C (10°C/min)

The weight changes in the temperature ranges of 350–415°C and 285–350°C are obtained (denoted as TG-a (%) and TG-b (%), respectively).

Table 1 Composition of slag samples ¹⁷⁾

	(mass%)							
	Ca	Fe	Si	Mn	Mg	Al	P	S
Slag A	32.0	21.5	6.3	3.2	1.4	1.6	0.8	N. D.
Slag B	29.9	22.9	6.5	2.8	3.6	1.5	0.9	N. D.
Slag C	30.6	22.4	6.2	2.4	3.8	1.7	1.0	N. D.
Slag D	30.8	21.7	5.9	2.3	3.6	1.2	1.1	N. D.

N. D.: Not detected

(3) Calculation of amounts of MgO and Mg(OH)₂

The amounts of Mg(OH)₂ and free-MgO are calculated from the results obtained by TG measurements by the following equations.

-Calculation of Mg(OH)₂

$$\text{Mg(OH)}_2 = \text{TG-a (\%)} - \text{TG-b (\%)}$$

Mg as Mg(OH)₂ is obtained.

-Calculation of free-MgO

$$[\text{Mg as free-MgO}]$$

$$= [\text{Mg as (MgO+Mg(OH)}_2)] - [\text{Mg as Mg(OH)}_2]$$

3. Results and Discussion

3.1 Form of Existence of Mg in Slag

In order to clarify the Mg compounds contained in slag, a microstructural analysis was performed by a scanning electron microscope (SEM)-energy dispersive X-ray spectrometer (EDX). The Mg in the slag was detected at the same positions as O, Fe, Si and Al. From this, the main forms of Mg in steelmaking slag were estimated to be complex oxides compounded oxides or hydroxides of Mg with Fe, Si and Al. As Mg was not detected at the same positions as P or S in the samples used here, it is thought that phosphates, sulfides and sulfates were virtually nonexistent. Based on these results, the reagents shown in section 2.1.1 were selected as substances for use in study of an chemical extraction method for Mg compounds in slag.

3.2 MgO and Mg(OH)₂ Dissolution Method

In the analytical method of CaO and MgO in cement clinker¹⁴⁾, 2.5 mass% of I₂ is added to EG, and CaO and MgO are determined from the change in electrical conductivity. In analysis of inclusions in metals^{15,16)}, a 10–20 mass% I₂-alcohol solution is used; however, depending on the kinds of metal, the optimum I₂ concentration, solvent composition, dissolution temperature and dissolution time differ, and solubility also changes. Therefore, first, the possibility of chemical extraction of MgO by an I₂-ethanol (C₂H₅OH) solution was studied by using reagents of MgO, Mg(OH)₂ and various complex oxides, which are the main forms of Mg in slag.

3.2.1 Dissolution of Mg compounds using reagents

The dissolution rate of MgO was determined by stepwise addition of a saturated I₂-C₂H₅OH solution (25 mass% I₂-C₂H₅OH) to EG. In this study, 10 mg of the MgO reagent was used. The dissolution rate was investigated by adding a solution, in which the combined I₂-C₂H₅OH solution and EG were adjusted to a constant 25 ml, to the MgO reagent. The heating conditions were 80°C × 60 min. The results are shown in

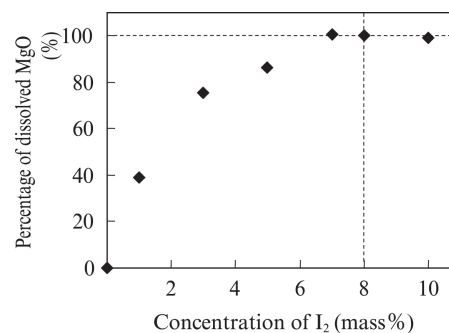


Fig. 1 Effect of concentration of I₂ for dissolution of MgO (MgO: 10 mg, Solvent: 25 ml of I₂-C₂H₅OH-ethyleneglycol, Temperature: 80°C, Heating time: 60 min)¹⁷⁾

Fig. 1.

Because 100% of the MgO was dissolved when the I₂ concentration of the solution was 7 mass% or more, the necessary solution concentration for dissolution of MgO was decided to be 8 mass% I₂-24 mass% C₂H₅OH-EG. The solubility of Mg compounds was investigated using this solution. As a result, it was found that MgO and Mg(OH)₂ are almost completely dissolved by the above-mentioned solution, whereas complex oxides of Mg compounded with Fe, Si and Al, which are the other main forms of Mg in slag, are substantially not dissolved. Based on this, 8 mass% I₂-24 mass% C₂H₅OH-EG was adopted as the solution for dissolution of MgO+Mg(OH)₂ in steelmaking slag.

3.2.2 Optimization of dissolution conditions for MgO and Mg(OH)₂ by using simulated slag

A simulated slag for use in study of MgO dissolution was prepared. The simulated slag was prepared by melting a mixture of reagents of CaCO₃, SiO₂, Al₂O₃ and MgO, and cooling and crushing the resulting material. The total Mg content in the synthesized simulated slag was 10.6 mass%. Using this simulated slag, the optimum temperature and time for dissolution of MgO in slags in the 8 mass% I₂-24 mass% C₂H₅OH-EG solution was studied. The results are shown in Fig. 2.

The amount of Mg dissolution from the simulated slag became constant when the dissolution temperature

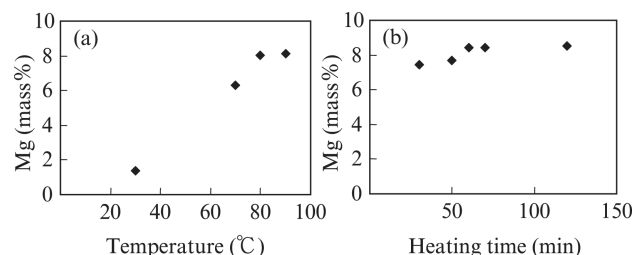


Fig. 2 Effect of (a) heating temperature and (b) heating time on dissolution of MgO in slags (Slag: 0.1 g, Solvent: 25 ml of 8 mass% I₂-24 mass% C₂H₅OH-ethyleneglycol)¹⁷⁾

was 80°C or higher and the dissolution time was 60 min or longer. The conditions for dissolution of MgO and Mg(OH)₂ in 8 mass% I₂-24 mass% C₂H₅OH-EG were set at 80°C and 60 min.

3.3 Determination of Mg(OH)₂ by Thermogravimetric Analysis

The sum of the concentrations of MgO and Mg(OH)₂ can be determined by ICP-AES analysis of the Mg in the solution dissolved with 8 mass% I₂-24 mass% C₂H₅OH-EG. Although direct determination of MgO is difficult by this method, the content of MgO can be determined by subtracting the amount of Mg(OH)₂ from sum of the concentrations of MgO and Mg(OH)₂. Therefore, a method for determination of Mg(OH)₂ by TG was studied. Because the amount of Ca(OH)₂ in steelmaking slag is generally larger than the amount of Mg(OH)₂, the existence of Ca(OH)₂ is an influence to accuracy when measuring Mg(OH)₂ in slag by TG. In steelmaking slag, a decrease in weight occurs accompanying thermal decomposition of Ca(OH)₂ at 400–460°C, as shown by the dotted line in Fig. 3. The pyrolysis temperature of Mg(OH)₂ is 350–415°C, which overlaps the decomposition temperature of Ca(OH)₂. In order to reduce the influence of Ca(OH)₂ on determination of Mg(OH)₂, it is possible to use a sample from which Ca(OH)₂ has been removed from the slag sample in advance in the TG analysis. Therefore, for this measurement method, we examined the possibility of using samples from which Ca(OH)₂ is removed by EG, conforming to the method of dissolving CaO in slag⁵⁾. The TG curve after EG treatment is shown by a solid line in Fig. 3.

Because the weight decrease which accompanies pyrolysis of Ca(OH)₂ is no longer observed when the slag is treated with EG, it can be understood that Ca(OH)₂ has been removed. As a result, highly accurate determination of Mg(OH)₂ in slag by TG is possible by measuring the weight reduction at 350–415°C with an EG treated sample, and simultaneously with this, performing compensation by treating the weight loss at

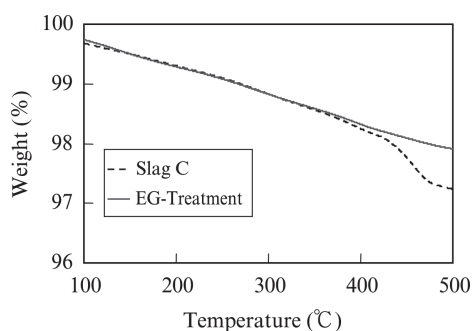


Fig. 3 Thermogravimetry curves of slag C before and after the treatment with ethyleneglycol (Slag: 0.1 g, Heating rate: 10°C/min, Atmosphere: Ar)¹⁷⁾

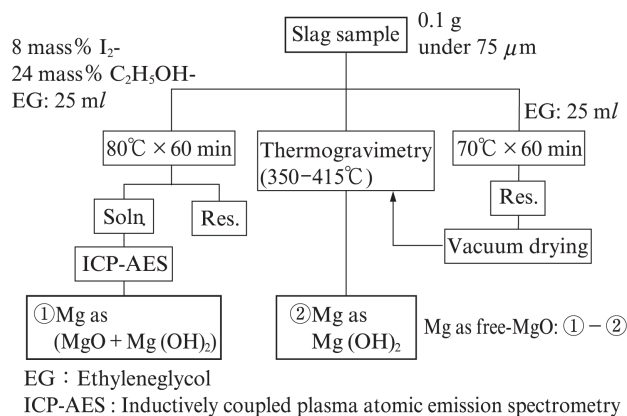


Fig. 4 Scheme of analytical methods for free-MgO in slags¹⁷⁾

285–350°C as background. The average of three analytical values of Mg(OH)₂ in actual slag C was 0.054 mass%, and the standard deviation (σ) was 0.008 mass%, showing sufficient accuracy for practical purposes.

3.4 Scheme of Developed Free-MgO Analysis Methods

Figure 4 shows an outline of the analytical methods for free-MgO in steelmaking slag developed as a result of the study described above.

3.5 Determination of Free-MgO in Steelmaking Slag

Table 2 shows the results of determination of the MgO content in three sample slags by the developed method. The three slags shown here are slag A, which is an actual slag, and slag A' and slag A'', which were prepared by adding 1 mass% and 5 mass% of reagent MgO, respectively, to slag A.

The free-MgO in slag A was determined to be 1.10 mass% by this analytical method. The analytical value of MgO in slag A', which was prepared by adding 1 mass% of MgO to slag A, was 2.12 mass%, and the value for slag A'', containing 5 mass% of added MgO, was 6.06 mass%. Thus, the rates of recovery from the added MgO were 102% and 99%, respectively. It can be understood that a known amount of MgO added to slag can be determined with good accuracy. These results demonstrate that determination of free-MgO in slag is possible by the developed method.

The free-MgO contents in slags B, C and D were also

Table 2 Analytical results of free-MgO in slag A¹⁷⁾

	Total Mg (mass%)	Added MgO (mass%)	Mg(OH) ₂ (mass%)	free-MgO (mass%)	Recovery (%)
Slag A	1.42	—	< 0.01	1.10	—
Slag A'		1.0	< 0.01	2.12	102
Slag A''		5.0	< 0.01	6.06	99

Table 3 Analytical results of free-MgO in slags¹⁷⁾
(mass%)

	Total Mg		① Mg as (MgO + Mg(OH) ₂)	② Mg as Mg(OH) ₂	Mg as free-MgO
Slag B	3.6 ₄	Ave.	0.43 ₄	< 0.01	0.43
		σ	0.03 ₃	—	
Slag C	3.8 ₃	Ave.	0.48 ₇	0.05 ₄	0.43
		σ	0.00 ₅	0.00 ₈	
Slag D	3.5 ₆	Ave.	0.27 ₄	< 0.01	0.27
		σ	0.01 ₃	—	

determined by the developed method. The results are shown in **Table 3**.

The table shows the average (Ave.) and standard deviation (σ) of the analytical results when analysis of each sample was performed repeatedly three times. With all the samples, the relative standard deviation of the repeatability of the analytical values of Mg as (MgO+Mg(OH)₂) was 10% or less, showing satisfactory analytical precision. It can be said that highly accurate determination of MgO+Mg(OH)₂ and MgO in slag at the 0.1 mass% level is possible by this method. Moreover, although there was virtually no difference in the total Mg in slags B-D, analysis by the developed method revealed a large difference in the contents of free-MgO in slags B and C and in slag D.

4. Conclusion

An analytical method for free-MgO in steelmaking slag was studied, and a method for determination of Mg(OH)₂ was developed based on a combination of a fractional dissolution method for [MgO+Mg(OH)₂] by dissolution with I₂-ethyleneglycol (EG), and thermo-

gravimetric analysis of the sample after EG treatment. The content of free-MgO is obtained from the difference between the two results. This method enables evaluation of free-MgO in slag. It is possible to apply this technique to studies of aging treatment conditions, indexes of criteria for judging that shipment of slag is possible, and other fields.

References

- 1) JIS A 5015. Iron and steel slag for road construction. 2013.
- 2) Narita, K.; Onoye, T.; Takata, Z. Tetsu-to-Hagané. 1978, vol. 64, p. 1558.
- 3) Suito, H.; Yokomaku, T.; Hayashida, Y.; Takahashi, Y. Tetsu-to-Hagané, 1977, vol. 63, p. 2316.
- 4) Sasaki, M.; Niida, A.; Otsuki, T.; Tsuchiya, K.; Nagao, Y. Tetsu-to-Hagané. 1982, vol. 68, p. 641.
- 5) The Japan Iron and Steel Federation, Committee for Utilization of Slag and Expert Committee on Steel Slag. Tentative Method of Analysis of Free Lime in Converter Slag and Electric Furnace Slag. 1980.
- 6) The Iron and Steel Institute of Japan. Standardization of analytical methods for characterization of free-CaO in steel slag. Final Report, 2013.
- 7) Inui, M.; Oda, M.; Tanaka, T. Bull. Iron Steel Inst. Jpn. 2014, vol. 19, p. 569.
- 8) Nishinohara, I.; Kase, N.; Maruoka, H.; Hirai, S.; Eba, H. Tetsu-to-Hagané. 2013, vol. 99, p. 552.
- 9) Tanaka, K.; Narita, M.; Watanabe, K. Tetsu-to-Hagané. 2014, vol. 100, p. 1386.
- 10) Fujioka, Y.; Aimoto, M.; Nishifuji, M. CAMP-ISIJ. 2009, vol. 22, p. 683.
- 11) Aryunan, P.; Kumar, A. Cem. Conc. Res. 1994, vol. 24, p. 343.
- 12) Kanehashi, K.; Aimoto, M. Tetsu-to-Hagané. 2013, vol. 99, p. 543.
- 13) Nishifuji, M.; Aimoto, M.; Fujioka, Y. Annual Meeting of the Japan Society for Analytical Chemistry. 2013, vol. 62, p. 3120.
- 14) Yu, J. H.; Wu, X. Fenxi Huaxue. 1998, vol. 26, p. 1075.
- 15) Maekawa, S.; Ebihara, M. Bunseki Kagaku. 1957, vol. 6, p. 715.
- 16) Maekawa, S. Tetsu-to-Hagané. 1969, vol. 55, p. 381.
- 17) Hanada, K.; Inose, M.; Sato, S.; Watanabe, K.; Fujimoto, K. Tetsu-to-Hagané. 2016, vol. 102, p. 24.